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Articles are published in Uzbek, Russian, and English, ensuring a wide-reaching audience and fostering cross-cultural academic exchange. As a beacon of academic excellence, the "Journal of Transport" continues to serve as a vital conduit for knowledge dissemination, collaboration, and innovation in the transport sector and related fields.

Requirements for attachments for sliding rail lashes of seamless track

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Abstract: The article is devoted to the determination of the technical parameters of the design of attachments for the production of works on laying rail lashes of a seamless track. The goal is set and the task of the study is formulated. The problem is solved by the simulation method. In the Femap with NX Nastran software package, a finite element model of a rail string was developed, which makes it possible to assess the stress-strain state of the rail strings when they are pushed onto the under-rail supports. During calculations, the model of the rail string is loaded in accordance with the data of the technological process (lifting and shifting of the rail string), as a result, the reaction forces at the points of load application are determined. Based on the reaction forces, technical requirements for attachments are established. Validation calculations were made to check the reliability of the model.

Keywords: jointless track, rail string, hinged equipment, technical requirement, modeling

Uloqsiz yo'lining rels pletlarini surishda ishlatiladigan osma moslamalariga qo'yiladigan talablar

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Annotatsiya: Maqola uloqsiz yo'lining rels pletlarini yotqizish ishlarini bajarish uchun osma moslamalar konstruksiyasining texnik parametrlarini aniqlashga bag'ishlangan. Tadqiqotning maqsadi qo'yilgan va vazifasi shakllantirilgan. Qo'yilgan masala modellashirish usuli bilan yechilgan. Femap with NX Nastran dasturiy majmuasida rels pletlarini rels osti tayanchlariga surishda ularning kuchlanganlik-deformatsiya holatini baholash imkonini beruvchi rels pletining chekli elementli modeli ishlab chiqilgan. Hisoblashlarda rels pletining modeli texnologik jarayon (rels pletining ko'tarilishi va siljishi) ma'lumotlariga muvofiq yuklanadi, natijada yuklama qo'yilgan nuqtalardagi reaksiya kuchlari aniqlanadi. Reaksiya kuchlari asosida osma moslamalarga texnik talablar qo'yilgan. Modelning ishonchligini tekshirish uchun validatsion hisob-kitoblar amalga oshirilgan.

Kalit so'zlar: uloqsiz yo'l, rels plet, osma moslama, texnik talab, modellashirish

1. Kirish

Chet el temir yo'llarida yo'lni elementma-element yotqizishda kombinatsiyalashgan yurishli ekskavatorlar keng qo'llaniladi. Har xil osma uskunalar (osma moslamalar) bilan jihozlangan bu turdagi mexanizatsiya har xil turdagi yo'l ishlari uchun, shu jumladan rels pletlarini yotqizish uchun ham qo'llanilishi mumkin. So'nggi yillarda O'zbekiston [1] va Rossiya [2] temir yo'llarida rels pletlarini almashtirish uchun shunga o'xshash texnologiyalarni joriy etish boshlandi. Joriy etishning dastlabki natijalari bunday texnologiyani qo'llashning yuqori samaradorligini ko'rsatdi. Uning qo'llanilish sohasini kengaytirish uchun inventar relslarni payvandlangan rels pletlariga almashtirish imkonini beruvchi ikkitali g'ildirakli rels ushlagich konstruksiyasi [3] taklif etilgan. Me'yoriy adabiyotlarni tahlil qilish natijasida uloqsiz yo'lining rels pletlarini yotqizish ishlarini bajarishda moslamaning xavfsiz ishlashini ta'minlaydigan texnik talablar aniqlanmagan.

Ushbu ishning maqsadi inventar relslarni payvandlangan rels pletlariga almashtirishni amalga oshiradigan osma

moslamalar konstruksiyalariga texnik talablarni belgilashdan iborat.

Qo'yilgan maqsadga erishish uchun ishlarni bajarish jarayonida rels va osma moslamalarga ta'sir etuvchi kuchlarni aniqlash lozim.

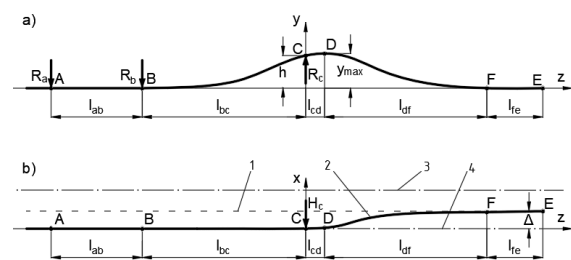
2. Tadqiqot metodologiyasi

Osma moslama bilan jihozlangan kombinatsiyalashgan yurishdagi ekskavatorni qo'llagan holda rels pletlarini yotqizish texnologiyasi quyidagicha amalga oshiriladi: ekskavator strelasini oldinga yo'naltirgan holda harakatlanib, avval bitta rels ipini, so'ngra (yo'l bo'ylab qayta teskari yo'nalishda o'tganda) ikkinchi rels ipini yotqizadi. Yotqizishdan oldin inventar relslar oldindan olib tashlanadi (siljiriladi), avval bitta ip bo'yicha, keyin esa ikkinchisi bo'yicha, ya'ni inventar relslar olib tashlangandan so'ng, darhol ularning o'miga bitta ip bo'yicha rels pletlari joylashtiriladi, keyin xuddi shunday ish ikkinchi rels ipi bo'yicha amalga oshiriladi [4]. Ishlarni bajarishning

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tavsiflangan texnologiyasiga mos keladigan hisoblash sxemasi 1-rasmda keltirilgan.



1-rasm. Hisoblash sxemasi:

a - rels pletining vertikal tekislikdagi egilishi; b - rels pletining gorizontaal tekislikdagi egilishi;

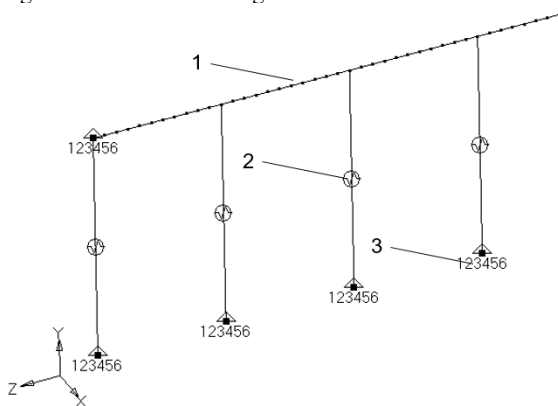
1 - rels pletining surilishgacha bo'lgan holati; 2 - rels pletining surilishdan keyingi holati; 3 - yo'l o'qi; 4 - rels ipining o'qi

Yuk qo'yilish nuqtasidagi R_c va H_c reaksiya kuchlarini aniqlash zarur.

Rels pletlarini yuklash va tushirishda yuk qo'yilgan nuqtadagi reaksiya kuchlarini aniqlash bilan bog'liq masalalar V.Ya. Shulga [5], S.P. Pershin [6], V.P. Shramenko [7] va V.V. Yershov [8] tomonidan yechilgan. [5] ishda R50 relslaridan payvandlangan rels pletlarini ma'lum balandlikka ko'tarishda tajriba yo'li bilan, [6] ishda R50 relslari uchun hisoblash yo'li bilan, [7] ishda R65 relslari uchun hisoblash va tajriba yo'li bilan, [8] ishda R65 rels uchun hisoblash yo'li bilan aniqlangan.

Masalani yechish uchun Femap with NX Nastran dasturiy majmuasida rels pletining chekli elementli modeli modellashtirildi.

Femap with NX Nastran dasturiy majmuasida rels pletini modellashtirishda Beam chekli element turi tanlangan. Modelning uzunligi 147,4 metrni tashkil qiladi. Modelda rels pletlari va shpalla orasidagi kontakt Spring/Damper elementi yordamida amalga oshirildi, ularning o'ziga xos xususiyati qo'yilgan kuchlarga nisbatan ko'chishlarning chiziqli bo'lmagan funksional bog'liqliklarini oltita erkinlik darajasi bo'yicha berish imkoniyati hisoblanadi: o'qlar bo'ylab uchta yo'nalish va o'qlarga nisbatan burchakli ko'chishlarning uchta bog'liqligi. Femap with NX Nastran dasturiy majmuasida rels pletining chekli elementli modeli fragmenti 2-rasmda keltirilgan.



2-rasm. Rels pletining chekli elementli modeli fragmenti:

1 - relsni modellashtiruvchi Beam turidagi element; 2 - rels va shpalla orasidagi kontaktni modellashtiruvchi Spring/Damper turidagi element; 3 - erkinlik darajalarini mahkamlash

Yuklar model tugunlariga kuchlar va belgilangan siljish shaklida uzatildi.

Hisoblash uchun nochiziqli statik tahlil (Nonlinear Static) usuli qabul qilingan.

3. Natija va muhokamalar

Hisoblarni bajarish dastlabki ma'lumotlar sifatida quyidagilar qabul qilindi:

- 1) ko'tarilish balandligi: 0,1, 0,15, 0,2 va 0,25 m;
- 2) strelaning qulochi: 5,32, 5,82, 6,32 va 6,82 m;
- 3) siljish kattaligi $\Delta = 0,57$ m.

Hisoblash natijasida olingan yuklama qo'yilgan nuqtadagi reaksiya kuchlari 1 va 2-jadvallarda keltirilgan.

1-jadval

Yuk qo'yilgan nuqtadagi R_c reaksiya kuchlari

Strela qulochi, m	Ko'tarilish balandligidagi reaksiya kuchi, kg			
	0,10 m	0,15 m	0,20 m	0,25 m
5,32	3280	3859	4324	4711
5,82	2992	3552	3988	4362
6,32	2744	3287	3713	4061
6,82	2549	3052	3457	3798

2-jadval

Yuk qo'yilgan nuqtadagi H_c reaksiya kuchlari

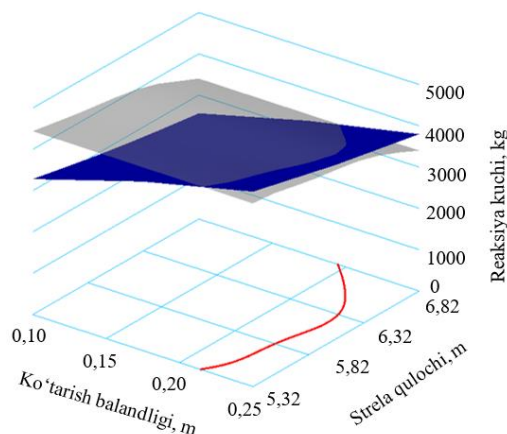
Strela qulochi, m	Ko'tarilish balandligidagi reaksiya kuchi, kg			
	0,10 m	0,15 m	0,20 m	0,25 m
5,32	503	515	526	496
5,82	473	489	484	466
6,32	448	468	470	465
6,82	426	445	455	450

Reaksiya kuchlarining vertikal tekislikdagi qiymatlari R_c (1-jadval) yuk qo'yilgan nuqtada ko'tarilish balandligi ortishi bilan ortadi, strelaning qulochi ortishi bilan esa, aksincha, kamayadi. Reaksiya kuchlarining maksimal qiymati kran strelasining eng yuqori ko'tarilish balandligida va strela qulochining minimal qiymatida erishiladi, hamda bu qiymat 4711 kilogrammga teng. 1-jadval ma'lumotlari asosida grafik qurilgan (3-rasm).

Gorizontaal tekislikdagi reaksiya kuchlarining (H_c) qiymatlari (2-jadval) ko'tarilish balandligi 0,1 m dan 0,2 m gacha ortishi bilan ortadi, ko'tarilish balandligi 0,2 m dan oshishi bilan kamayadi va strelaning qulochi ortishi bilan ko'tarilishning barcha qiymatlarida kamayadi. Bunda reaksiya kuchlarining qiymati 426-526 kg oralig'ida bo'ladi.

Yuk qo'yilgan nuqtadagi reaksiya kuchlari va 1,15 zaxira koeffitsiyentini hisobga olgan holda kombinatsiyalashgan yurishli ekskavatorning yuk ko'tarish qobiliyati 3-rasmda ko'rsatilgan [9]. Grafikdan ko'rinish turibdiki, strelaning qulochi 5,32, 5,82 va 6,32 metr bo'lganda ko'tarilish balandligi 0,2 metrdan oshsa, hamda qulochi 6,82 metr va ko'tarilish balandligi 0,2 metr bo'lganda, reaksiya kuchining qiymati kombinatsiyalashgan yurishli ekskavatorning yuk ko'tarish qobiliyatidan oshib

ketadi. Grafikning asosiga ikki sirtning kesishish chizig'i proyeksiyalangan. Grafik asosida proyeksiyalangan chiziq rels pletlarini almashtirish ishlarini xavfsiz bajarish uchun strelaning ko'tarish balandligi va qulochining nominal qiymatlarini aniqlash imkonini beradi. Grafikdan ko'rinib turibdiki, yuk ko'tarish qobiliyatining eng katta zaxirasi 0,2-6,32 (ko'tarish balandligi va strelaning qulochi) konfiguratsiyalarda kuzatiladi.



3-rasm. Yuk qo'yilgan nuqtadagi reaksiya kuchlari grafigi: (ko'k - reaksiya kuchlari, kulrang - ekskavatorning yuk ko'tarish qobiliyati)

Ko'tarish balandligining nominal qiymatini bilgan holda osma moslamaning yuk ko'tarish qobiliyati va massasi aniqlanadi. Grafikdan (3-rasm) ko'rinib turibdiki, ko'tarish balandligi 0,2 m bo'lganda yuk ko'tarish qobiliyati bo'yicha eng kichik zaxira strela qulochi 5,32 m bo'lganda kuzatiladi. Shunga ko'ra, bu holatda reaksiya kuchi 4324 kilogrammni tashkil etadi. Yuk ko'tarish mexanizmlari uchun ishonchlilik koeffitsiyenti 1,34 [10] ni hisobga olgan holda, osma moslamaning yuk ko'tarish qobiliyati 5794 kg dan kam bo'lmasligi kerak. [11] talablarini hisobga olgan holda osma moslamaning yuk ko'tarish qobiliyatining nominal qiymati 6300 kg ga teng deb qabul qilinadi. Xuddi shu konfiguratsiya uchun kombinatsiyalashgan yurishli ekskavatorning [9] reaksiya kuchi va yuk ko'tarish qobiliyati o'rtasidagi farq 126 kg ni tashkil etadi, shundan kelib chiqqan holda, osma uskunaning massasi 126 kg dan oshmasligi kerak.

Modelni validatsiya qilish, shuningdek, hisoblash natijalarini tekshirish uchun ishlab chiqilgan rels pletining modeli [7] ishda keltirilgan rels pletlarini harakatlanuvchi tarkibdan tushirish jarayonida ularning kuchlanganlik-deformatsiya holati ma'lumotlariga muvofiq yuklandi. Hisoblash natijalari 3-jadvalda keltirilgan.

3-jadval

Hisoblash natijalarini solishtirish

№	Yuklash bosqichlari*	Reaksiya kuchlari, kg		Farq, %
		[7] bo'yicha	hisob bo'yicha	
1	1.b-rasm, R_0	2334	2288	2,0
2	1.b-rasm, R_b	355	360	1,4
3	1.b-rasm, R_a	620	724	16,8

Izoh: yuklanish bosqichlari [7] bo'yicha rasmlarning raqamlanishiga mos keladi

Ishlab chiqilgan modelni tekshirish jarayonida olingan qiymatlarni taqqoslash (3-jadval) shuni ko'rsatadiki, [7] bo'yicha reaksiya kuchlarining qiymatlari va hisoblangan qiymatlar bir-biriga mos keladi. Reaksiya kuchlari qiymatlari orasidagi maksimal og'ish 16,8% dan oshmaydi.

4. Xulosa

Amalga oshirilgan hisob-kitoblar natijasida osma moslamaning nominal yuk ko'tarish qobiliyati va massasi aniqlandi. Bu ma'lumotlar uning konstruksiyasini ishlab chiqishda e'tiborga olinishi lozim.

Chekli elementli modellashirish muhitida olingan natijalarni analitik tenglamalar asosida bajarilgan o'xshash hisob-kitoblar bilan qiyosiy tahlil qilish shuni ko'rsatdiki, natijalar qoniqarli darajada o'zaro mos keldi. Bu esa ishlab chiqilgan modelning yetarlicha to'g'ri ekanligini va uni qo'llash doirasini kengaytirish mumkinligini tasdiqlaydi.

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