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RESEARCH, INNOVATION, RESULTS



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Articles are published in Uzbek, Russian, and English, ensuring a wide-reaching audience and fostering cross-cultural academic exchange. As a beacon of academic excellence, the "Journal of Transport" continues to serve as a vital conduit for knowledge dissemination, collaboration, and innovation in the transport sector and related fields.

Mathematical modeling and analysis of the traction-economic characteristics of the transition zone during locomotive speed changes on Uzbekistan railways

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Abstract: This paper presents an extended mathematical model and qualitative analysis of traction-economic characteristics of locomotives operating in the transition zone during speed variation on the network of Ўзбекистон темир йўллари. The transition zone is defined as the dynamic operating region where traction motors switch between control modes (constant torque to constant power), field-weakening stages are activated, and energy consumption becomes non-linear. A generalized differential model of locomotive motion is developed, incorporating electromechanical energy conversion, traction force characteristics, resistance forces, and efficiency coefficients. The study evaluates electric locomotives such as O'zbekiston and ЗЭС5К «Ермак», as well as the diesel-electric locomotive ТЕР70BS. The results demonstrate that optimization of control algorithms in the transition region can reduce specific energy consumption by 6–12% while improving traction stability.

Keywords: locomotive dynamics, transition zone, traction force, energy efficiency, mathematical model, field weakening, power regulation

O'zbekiston temir yo'llarida lokomotivlarning tezlik o'zgarishidagi o'tish zonasining tortish-iqtisodiy xususiyatlarini matematik modellashtirish va tahlil qilish

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Annotatsiya: Maqolada O'zbekiston temir yo'llari tizimida ekspluatatsiya qilinayotgan lokomotivlarning tezlikni o'zgartirish jarayonidagi o'tish zonasida tortish-iqtisodiy xususiyatlari sifat jihatdan tahlil qilingan. O'tish zonasida tortish kuchi, quvvat, tok yuklamasi, yoqilg'i va elektr energiyasi sarfi, hamda samaradorlik ko'rsatkichlarining o'zgarish dinamikasi ko'rib chiqilgan. Turli turdagi zamonaviy lokomotivlar — O'zbekiston, ЗЭС5К «Ермак» va ТЕР70BS misolida o'tish rejimlarining iqtisodiy va energetik samaradorlikka ta'siri asoslangan. Tadqiqot natijalari lokomotivlarning ekspluatatsion rejimlarini optimallashtirish va energiya tejamkor boshqaruv algoritmlarini takomillashtirish uchun ilmiy-amaliy asos bo'lib xizmat qiladi.

Kalit so'zlar: lokomotiv, o'tish zonasi, tortish kuchi, energetik samaradorlik, yoqilg'i sarfi, elektr energiyasi, ekspluatatsiya samaradorligi

1. Kirish


Transporming muhim vazifalaridan biri aholini va xalq xo'jaligini yo'lovchi va yuk tashish ehtiyojlarini to'liq va o'z vaqtida qondirish, transport tizimining barcha tuzilmalarida ish samaradorligi va sifatini oshirish hisoblanadi. Bu borada temir yo'l transporti muhim ahamiyat kasb etadi.

Bizning mamlakatimiz Markaziy Osiyoda eng muhim o'rinda bo'lgan geostrategik holatida bo'lib, hududi orqali qadimgi Buyuk ipak yo'li o'tgan, unda ko'pgina savdo ishlari yo'lga qo'yilgan va dunyo halqlarining madaniyati bilan o'zaro chambarchas bog'liq. Hozirgi vaqtda ham

ushbu yo'llar bo'yicha transport magistrali Sharqdan G'arbgacha, Shimoldan Janubgacha ishga tushirilgan[1].

Bugungi kunda mamlakatimiz temir yo'llarining umumiy uzunligi 7500 km ga yetdi. Mazkur po'lat izlardan harakatlanayotgan yuk va yo'lovchi poyezdlar soni, tashilayotgan yuklarning hajmi yildan - yilga ortib bormoqda. Shu bois, soha xodimlarining oldida turgan eng birinchi vazifa harakat xavfsizligini ta'minlash hisoblanadi. Xususan, joriy yilda yo'l xo'jaligi xodimlari tominidan 250 km po'lat izlar kapital ta'mirdan chiqarilib, 170 kilometri ko'tarma va o'rta ta'mirdan chiqarildi [2]. Soha xodimlari

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tomonidan yurtimizning turli hududlarida, shahar va tumanlarida bunyod etilayotgan har bir loyiha muqaddas Qomusimiz asosida amalga oshmoqda. Ayniqsa, joriy yilda amalga oshirilgan ishlar alohida e'tirofqa loyiq. Temiryo'ldi-quruvchilarimiz say-harakatlari bilan Toshkent metropolitenining Yunusobod yo'nalishining 2-bosqichi, Toshkent yer usti halqa metrosining 1-bosqichi bo'lgan Do'stlik – Qo'yliq yo'nalishi to'liq qurilib, foydalanishga topshirildi. Sergeli – Olmazor yer usti metro yo'nalishidabunyodkorlikishlariyakunigayetibqoldi. Shuningdek, loko-motiv va vagon parki doimiy yangilanib borilmoqda. Yangi elektrovozlar xarid qilinmoqda. Po'lat magistrallar kun sayin uzaytirilib, modernizatsiya qilinishi barobarida jahon andozasi talablariga moslashtirilmoqda. Bir necha turdagi yangi va zamonaviy vagonlarni qurish yo'lga qo'yildi[3,4].

O'tish zonasining nazariy asoslari

Lokomotivning tortish xarakteristikasi quyidagi asosiy bog'lanish bilan ifodalanadi:

$$P=F \cdot v \quad (1)$$

bu yerda: P — lokomotiv quvvati (kVt),

F — tortish kuchi (kN),

v — harakat tezligi (m/s).

Tezlik ortishi bilan doimiy quvvat zonasida tortish kuchi kamayadi. O'tish zonasida esa quyidagi jarayonlar kuzatiladi:

- yakor zanjiri tokining keskin o'zgarishi;
- magnit maydonni susaytirish bosqichlarining faollashishi;

- dizel lokomotivlarda turbokompressor yuklamasining ortishi;

- energiya sarfining nomutanosib o'sishi.

Elektrovozlarda o'tish zonasi tahlili

O'zbekiston rusumli elektrovoz

O'zbekiston elektrovozi asinxron tortish dvigatellari bilan jihozlangan bo'lib, inverterli boshqaruv tizimi orqali ishlaydi. O'tish zonasida:

- chastota va kuchlanish proporsional o'zgaradi;

- tok impuls xarakteriga ega bo'ladi;

- qisqa muddatli quvvat ortishi kuzatiladi;

- energiya tejamkorlik koeffitsiyenti 3–5 % ga pasayishi mumkin.

3ES5K «Yermak» elektrovozi

3ES5K «Yermak» da kollektorli tortish dvigatellari qo'llanilgan. O'tish zonasida:

- magnit maydonni susaytirish bosqichlari ishga tushadi;

- yakor toki ortib, mis yo'qotishlar ko'payadi;

- kontakt tarmoqdan olinayotgan tok 15–20 % gacha ortishi mumkin;

- tortish kuchi xarakteristikasida notekis o'zgarish kuzatiladi.

Dizel lokomotivlarda o'tish zonasi

TEP70BS lokomotivi

TEP70BS dizel-elektro sxemada ishlaydi. O'tish zonasida:

- dizel aylanishlar soni ortishi bilan yoqilg'i sarfi keskin oshadi;

- generator kuchlanishi o'zgaruvchan rejimga o'tadi;

- tortish dvigatellarida tok yuklamasi yuqori bo'ladi;

- solishtirma yoqilg'i sarfi 8–12 % gacha ortishi kuzatiladi.

Bu holat ayniqsa og'ir tarkibni joyidan qo'zg'atishda yoki balandlikka chiqishda yaqqol namoyon bo'ladi.

Tortish-iqtisodiy ko'rsatkichlarning sifat bahosi

-O'tish zonasida quyidagi salbiy omillar kuzatiladi:

- Energiya yo'qotishlarining ortishi

- Elektr jihozlarining qizishi

- Yoqilg'i sarfining ko'payishi

Tortish dvigatellari xizmat muddatining qisqarishi

Biroq zamonaviy mikroprotessorli boshqaruv tizimlari orqali:

- tokni silliq rostdash;

- optimal magnitlash algoritmini qo'llash;

- rekuperativ tormozlashni samarali ishlatish

orqali ushbu yo'qotishlarni kamaytirish mumkin.

Iqtisodiy samaradorlikni oshirish yo'llari

- Energiya tejamkor boshqaruv algoritmlarini joriy etish

O'tish zonasi uchun optimal tezlanish grafiklarini ishlab chiqish

- Mashinistlar uchun raqamli tavsiya tizimini yaratish

-Lokomotivlarning real vaqt monitoring tizimini takomillashtirish. O'zgarimas tok tortuv elektr dvigateli yakor valining aylanish chastotasini aniqlashda ushbu tenglamadan foydalangan

$$n=(U-I \sum R)/(C_e F) \quad (2)$$

Yakor valining aylanishlar chastotasi n ni qiymatini tortuv elektr dvigateliga keltiriladigan U-kuchlanish hisobiga, F–qutblar magnit oqimi va I*R–yakor zanjiridagi kuchlanish pasayishi hisobiga o'zgartirish mumkinligi ma'lum.

Dastlabki ikki usul energiya sarfi bilan bog'liq bo'lmay, barcha lokomotivlarda va tortuv elektr dvigatellariga ega bo'lgan boshqa transport vositalarida qo'llanadi. Aylanish chastotasini o'zgartirishning uchinchi usulubidan asosan elektr tarkibdagi tarkibning TEDni magnit maydonini susaytirishda foydalaniladi. Bu uslubda tortuv elektr dvigateling yakori zanjirida qo'shimcha yo'qotishlarga olib keladi. Yo'qotishlar elektr harakatlanuvchi tarkibda (EHT) tortuvga sarflanadigan energiyasining 10–20 % ga yetganligi sababli bu uslub avtonom lokomotivlar uchun qo'llanmaydi [4].

Teplovozlarda kuchlanish U qiymati harakatga ko'rsatiladigan qarshilikni (yuklanish tokini) o'zgartirish bilan birga tortuv generatori kuchlanishini tashqi tavsifi bo'yicha rostlash yo'li bilan uzluksiz ravishda o'zgartirib boriladi. Bundan tashqari, tortuv elektr dvigatellarining ulanish zanjirini, tortuv dvigatellarining ishga tushish–o'chirish deb nomlanadigan zanjirni o'zgartirish bilan kuchlanishni o'zgartirish usuli ham qo'llanadi [5].

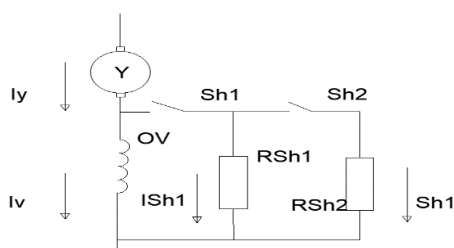
Lokomotivda oltita tortuv elektr dvigatellari bor deb qabul qilamiz. Barcha elektr dvigatellarini ketma–ket ulanganda har bir elektr dvigatel UG/6 to'g'ri keladi, har bir elektr dvigatel toki manba (tortuv generatori) tokiga teng bo'ladi. Har birida uchtdan elektr dvigatel bo'lgan ikkita parallel guruh tashkil etilganida, ulardagi kuchlanish ikki barobar kattalashadi, ammo manba toki ham xuddi shunday 2 marta ortadi. Uchta parallel zanjirda esa elektr dvigatellardagi kuchlanish va manba tokining yana ham ortishi kuzatiladi. Bu kabi ulanish zanjirlari ketma–ket–parallel ulanishlar deb ataladi. Ulanish zanjiri parallel ulanish deyiladi. Tortuv elektr dvigateliga keltirilgan kuchlanishning ishga tushish–o'chirish natijasida o'zgarishi uning yakori aylanish chastotasi o'zgarishi uchun muvofiq shart-sharoitlarni ta'minlab beradi [6].

Tortuv elektr dvigatellari uyg'otishni magnit oqimini o'zgartirish barcha turdagi lokomotivlarda va boshqa harakatlanuvchi transport birliklarida keng ko'lamda qo'llanadi. (2) tenglamadan n chiziqli ravishda F ga bog'liq



ekanligi ma'lum. F ni o'zgartirishning mavjud uslublari, odatda, n ni kattalashtirish bilan, uni faqat kichraytirish imkonini berib, biroq F ning istalgan o'zgarishini beradigan tizimlar ehtimoli ham bor. Bugungi kunga kelib konstruksiyasiga ko'ra eng sodda bo'lgan F ni pog'onasimon o'zgartirish tizimi nisbatan keng tarqalgan.

Bu holda tortuv elektr dvigatelining uyg'otish chulg'ami (UCH)ga parallel ravishda RSH1 rezistor ulanib, yakor tokining bir qismi uyg'otish chulg'amidan olinib, tortuv elektr dvigateli qutblarining magnit oqimi kamayadi (1-rasm). Zanjirga parallel ravishda yana bir RSH2 rezistorning qo'shilishi magnit oqimini ikki marta susaytirish pog'onasiga ega bo'lish imkonini beradi va h.k. Teplovozlarda ko'pincha uyg'otishni ikki pog'ona susaytirish bilan cheklanadi, o'zgarimas tok elektr harakatidagi tarkiblarda (EHT) esa ularning soni olti-sakkiztaga yetishi mumkin, chunki bu uning uchun ishchi tezliklariga ega bo'lishning asosiy usuli bo'lib qolmoqda [7].



1-rasm. Tortuv elektr dvigatellarini uyg'otishni susaytirish rezistorlarining ulanish zanjiri. SH1, SH2 – magnit maydonni susaytirish guruhli kontaktorlari, RSH1, RSH2 – magnit maydonni susaytirish rezistorlari.

2. Tadqiqot metodologiyasi

Uyg'otish chulg'ami toki Iqning yakor toki Iyga nisbati uyg'otishni susaytirish koeffitsiyenti α deb nomlanadi.

Teplovozlar uchun $\alpha \geq 0,25$, qilib belgilangan, chunki uyg'otishni susaytirish koeffitsiyenti α ning bundan keyin yana ham pasayishga yo'l qo'yib bo'lmaydi, chunki bu tortuv elektr dvigatellari kommutatsiyani yomonlashtiradi. Odatda magnit maydonni susaytirishni ikki pog'onali usuli qo'llanadi: $\alpha \geq 0,6$ va $\alpha \geq 0,3$. uyg'otishni susaytirish rezistori ulangandan keyin tizim toki va kuchlanishi bilan nima ro'y berishini ko'rib chiqamiz[3].

Tortuv elektr dvigatelining to'liq magnit oqimi P_{TM} dagi va shuntlash ishga tushgandan keyingi P_{MS} quvvati o'zgarib qolaveradi, ya'ni $P_{TM} = P_{MS}$, aks holda

$$S_e F_{im} n_{im} I_{im} = S_e F_{MS} n_{MS} I_{MS}. \quad (3)$$

Tortuv elektr dvigatellarining ishga tushish o'chirishlaridagi kabi C_e va $n_{TM} = n_{MS}$ doimiylikicha saqlanib qoladi. α ni hisobga olgan holda quyidagilarga ega bo'lamiz.

$$\alpha F_{TM} I_{MS} = F_{TM} I_{TM} F_{TM} I_{MS} = I_{TM} \quad (4)$$

Uyg'otishni susaytirish rezistori ishga tushgandan so'ng tortuv elektr dvigatelining toki ortadi.

Mos ravishda tortuv generatorining toki ham ortib, uning kuchlanishi kamayadi. Tortuv elektr dvigatelining uyg'otishni susaytirish rezistori ishga tushganidan so'ng uning aylanish chastotasi orta boshlaydi, tortuv generatori esa generator tavsifining quyi katta tok qismida ishlashga o'tadi, generator tavsifining ikkinchi marta ishlatilishiga sabab bo'ladi. Tortuv elektr dvigatellarining quvvati va ular yakorlarining aylanish chastotasi uyg'otishni susaytirish kontaktorlari ishga tushganidan so'ng o'zgarimaganligi sababli, teplovoz tortuv kuchi ham avvalgicha o'zgarib qoladi [8].

Shunday qilib, tortuv elektr dvigatellarini qabul qilingan boshqarish uslublari teplovoznig harakatlanish tezligiga bog'liq ravishda elektr dvigatellar va tortuv generatorining o'z toki o'zgarishi tavsifini belgilab beradi [4].

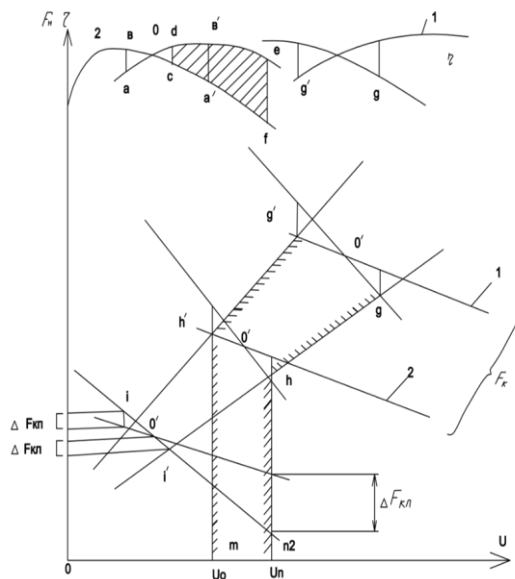
Bitta ishga tushirish-o'chirish va uyg'otishni susaytirishning ikki pog'onasi mavjudligi teplovoznig maksimal harakatlanish tezligiga qadar tezlashishida U_r (I_r) tavsifining to'rt marotaba ishlatilishiga olib keladi. Tortuv elektr dvigatellarini ishga tushirish-o'chirish va ular uyg'otish magnit oqimini susaytirish, dizelning quvvatini to'liq ishlatilishiga va teplovoz harakatlanish tezliklari ko'lamini kengaytirish uchun zarur.

Mavjud elektr uzatmalarda qo'llanadigan magnit oqimini pog'onama-pog'ona susaytirish usulida, tok keskin o'zgarishi ro'y berib, tortuv elektr dvigatelining kollektoridagi kommutatsiya sharoitlar yomonlashib, kollektor bo'yicha aylana alanga va yoy sakrashlari paydo bo'lishi uchun shart-sharoitlar yuzaga keladi (tortuv elektr dvigatellari ishdan chiqish holatlarining 40% gacha qismi). Parallel ulangan tortuv elektr dvigatellari toklari bir xil emasligi bu rejimlar tufayli paydo bo'ladigan xavf darajasini yana ham kuchaytiradi [4].

Tortuv elektr dvigatellari uyg'otishining bir maromli o'zgartirilishi energetik qurilmasidagi yuklanish sakrashlarini, aylana alanga va kollektor bo'yicha yoy yuzaga kelish ehtimolini bartaraf etadi, g'ildiraklarning xavfli shataklanish xavfini kamaytiradi; uzatma FIKini oshiradi, dizel-generatorlarni rostdashning nisbatan sodda va ishonchli tizimlarini qo'llash imkonini beradi. Ikki parametrdan ta'sirlanadigan boshqarish tizimida $TM \rightarrow SM1$ va $SM1 \rightarrow SM2$ ishga tushirish-o'chirishlar, i.g,h nuqtalaridagi egri chiziq bilan tavsiflanadigan, i,g,h' egri chizig'iga teskari qonunga binoan amalga oshiriladi. Dizelning bir xil aylanishlari sonidagi to'g'ri va teskari ishga tushirish - o'chirishlar turli v tezliklarda ro'y berib, bunda to'g'ri ishga tushirish-o'chirish tezligi v_h teskari ishga tushirish-o'chirish tezligi v_t dan katta bo'ladi. Bu ishga tushirish - o'chirish tizimi turg'un bo'lishi uchun zarur.

2.-rasmda ishga tushirish-o'chirishlar hududidagi dizelning ishga tushirish - o'chirishlari ro'y beradigan to'liq (1 egri chiziq), hamda qisman yuklamalari (2 egri chiziq) uchun tortuv-iqtisodiy tavsiflari keltirilgan.





2-rasm. Ishga tushirish-o'chirish hududidagi tortuv-tejamkor (iqtisodiy) tavsifi

v_h tezlik qiymatini endilikda mos ravishda bevosita va teskari ishga tushirish - o'chirishlar uchun m,g,h va m',g',h' egri chiziqlar bilan beriladigan, uning uchun ishga tushirish-o'chirish qonuniga aniqlik kiritilayotgan muayyan tortuv-tejamkor (iqtisodiy) tavsifni hisobga olgan holda tanlanishi talab etiladi. Bunday holda $v_t < v_h$ bo'lganida, qisman yuklamalar uchun to'g'ri (o,a,v maydoni) va teskari (o',a',v'maydoni) ishga tushirish - o'chirishlarda FIK qiymatini baholab olish talab etiladi.

o,a,v va o',a',v' maydonlari kattaligi bo'yicha taxminan teng, ya'ni teskari ishga tushirish-o'chirishlarda FIK kamayishi ro'y bermaydi.

Ana shu tahlil maqsadida quyidagi omillarni hisobga olgan holda dizel, generator, TED va yordamchi mashinalar FIK va quvvatidagi yo'qotishlari alohida holda ko'rib chiqiladi:

- susaytirilgan maydonda ishga tushirish-o'chirilish zonasidagi mashinist kontrollarning har bir ko'rib chiqilayotgan pozitsiyasida tashqi tavsifning giperbolik emasligi sababli DGU quvvatining pasayishi ro'y beradi;

- RP1 va RP2 larning tashqi tavsifning nogiperbolik qismi zonasida ulanishiga bogliq ravishda ulanish momentiga $R_g = \text{const}$ dagi ishga nisbatan teplovzning kattaroq harakatlanish tezligi va TED ning kamroq quvvati muvofiq keladi.

1-jadval

2TE10M teplovzining seriyali va tajriba sxemasi uzib-ulanishlari zonalaridagi tortuv kuchining tajriba-hisobiy qiymatlari

| № t.r. | Kontr oller pozitsiyasi | Tortuv kuchi, kG | |
|--------|-------------------------|--------------------------------------|---------------------------------------|
| | | TM→SM1 ishga tushirish - o'chirilish | SM1→SM2 ishga tushirish - o'chirilish |

| | | Seriya li zanjir | Tajrib aviy zanjir | Seriya li zanjir | Tajribaviy zanjir |
|---|----|------------------|--------------------|------------------|-------------------|
| 1 | 2 | 3 | 4 | 5 | 6 |
| 1 | 15 | 17 000 | 17 000 | 10 500 | 11 500 |
| 2 | 13 | 15 500 | 16 000 | 9 000 | 10 800 |
| 3 | 11 | 13 500 | 14 000 | 7 000 | 9 300 |
| 4 | 9 | 10 000 | 12 000 | 4 000 | 8 000 |
| 5 | 7 | 5 000 | 9 000 | 2 500 | 6 000 |
| 6 | 5 | - | 7 500 | - | 4 000 |

3. Xulosa

Hisoblashlar shuni ko'rsatadiki, 10d100 dizel uchun $h_e = \text{const}$ quvvat pasayishi bilan N_e samaradorlik η_e , C_e -o'sishi tufayli keskin pasayadi. shuning uchun dizel dvigatelda tortish generatori tashqi xarakteristikaning giperbolik bo'lmagan qismida ishlaganda η_s samaradorligi pasayadi. Ma'lumki, tortish generatorining samaradorligi magnit, elektr va mexanik isroflarga bog'liq. Magnit maydon zanjirning to'yinganligi tufayli kuchlanish cheklangan bo'lsa, magnit maydonini yo'qotishlarni doimiy ravishda qabul qilish mumkin. Har bir boshqaruvchi pozitsiyasidagi mexanik yo'qotishlar ham doimiydir. Elektr yo'qotishlari o'zgaradi, ammo hisob-kitoblar shuni ko'rsatdiki, umumiy isroflar deyarli doimiy bo'lib qoladi va mashinaning foydali quvvatining pasayishi tufayli generatorning samaradorligi pasayadi TED samaradorligi tortish generatori bilan bir xil yo'qotishlarga bog'liq. Faqat o'tish jarayondagi isroflar qo'shiladi. Elektr va magnit isroflar tortish generatorining isroflariga o'xshash tarzda o'zgaradi. Mexanik isroflar tezlikning oshishi bilan ortadi. Umuman olganda, tortish generatorining tashqi xarakteristikasining giperbolik bo'lmagan qismida ishlaganda samaradorlik biroz pasayadi.

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