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RESEARCH, INNOVATION, RESULTS



**TOSHKENT DAVLAT  
TRANSPORT UNIVERSITETI**

Tashkent state  
transport university



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# TASHKENT STATE TRANSPORT UNIVERSITY

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Articles are published in Uzbek, Russian, and English, ensuring a wide-reaching audience and fostering cross-cultural academic exchange. As a beacon of academic excellence, the "Journal of Transport" continues to serve as a vital conduit for knowledge dissemination, collaboration, and innovation in the transport sector and related fields.

## Investigation of the mechanism and factors influencing the process of dephosphorization during the smelting of 20GL steel

N.K. Tursunov<sup>1</sup><sup>a</sup>, A.A. Saidirakhimov<sup>1</sup><sup>b</sup>, N.K. Kodirova<sup>1</sup>, Z.F. Rakhmatova<sup>1</sup>

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**Abstract:** This article investigates the mechanism of the phosphorus refining (dephosphorization) process during the furnace melting of 20GL grade cast structural steel, as well as the main factors that influence it. Specifically, the standard Gibbs energy was derived based on the chemical reaction of the dephosphorization process, and the equilibrium constant was determined at various temperatures. Furthermore, the distribution coefficient of phosphorus between the metal and slag phases was studied in relation to the slag composition and quantity during the dephosphorization process. In this research, the interaction parameters of chemical elements within the metal on phosphorus activity were calculated. As a result of experiments and calculations, the activity and distribution coefficients of phosphorus were determined. The results obtained are of significant importance for improving the dephosphorization process in the production of 20GL grade cast steel.

**Keywords:** 20GL grade steel, refining, Gibbs energy, dephosphorization process, activity coefficient, distribution coefficient, slag basicity

## 20GL markali po'lat eritishda defosforatsiya jarayonining mexanizmi va ta'sir omillarini tadqiq etish

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**Annotatsiya:** Ushbu maqolada 20GL markali quyma konstruksion po'latni pechda eritish jarayonida fosfordan rafinirlash (defosforatsiya) jarayonini mexanizmi va unga ta'sir etadigan asosiy omillar tadqiq etilgan. Xususan, defosforatsiya jarayonini kimyoviy reaksiyasi asosida, standart Gibbs energiyasi keltirib chiqarildi hamda turli haroratlarda muvozanat konstantasi aniqlandi. Bundan tashqari metall va shlak fazalari o'rtasidagi fosforning taqsimlanish koeffitsiyenti defosforatsiya jarayonidagi shlak tarkibi va miqdori bo'yicha o'rganilgan. Tadqiqotda metall tarkibidagi kimyoviy elementlarning fosfor aktivligiga ta'sir parametrlari hisoblangan. Tajriba va hisob-kitoblarni natijasida fosforning aktivlik va taqsimlanish koeffitsiyenti aniqlangan. Olingan natijalar 20GL markali quyma po'latning ishlab chiqarishda defosforatsiya jarayonini takomillashtirish uchun muhim ahamiyatga egadir.

**Kalit so'zlar:** 20GL markali po'lat, rafinirlash, Gibbs energiyasi, defosforatsiya jarayoni, aktivlik koeffitsiyenti, taqsimlanish koeffitsiyenti, shlak asosililigi

### 1. Kirish


Bugungi kunda metallurgiya sanoati jadal rivojlanib borayotgan tarmoqlardan biri bo'lib, yuqori sifatli quyma konstruksion po'latlarga bo'lgan talab ortib bormoqda. Transport mashinasozligi, xususan, temir yo'l va avtomobilsozlik sohaslarida qo'llaniladigan mas'uliyatli detallar uchun yuqori darajadagi xavfsizlik, uzoq xizmat muddati, mustahkamlik, zarbiy qovushqoqlik hamda ishonchlilik xususiyatlariga ega bo'lgan materiallar talab etiladi. Shu nuqtai nazardan, mazkur tarmoqlarda keng qo'llaniladigan quyma po'latlar muhim konstruksion materiallardan biri hisoblanib, ularning sifati mexanik va texnologik xossalari, shuningdek, kimyoviy tarkibidagi legirolovchi elementlar ([Si], [Mn], [Cr], [Ni], [Ti], [Cu] va

bosh.) hamda zararli va keraksiz qo'shilmalar ([S], [P], [O], [N], [H]) miqdoriga bevosita bog'liqdir.

Zararli elementlar orasida fosfor alohida ahamiyatga ega bo'lib, u po'latning sovuq mo'rtligini oshiradi, plastiklik xossalari va zarbiy qovushqoqligini pasaytirib yorilishga moyillikni kuchaytiradi. Ayniqsa, harorat nisbatan past sharoitlarda ishlovchi detallar uchun fosfor miqdorini yuqori bo'lishi jiddiy muammo hisoblanadi. Shu sababli po'lat eritish jarayonida fosfor kamaytirish, ya'ni defosforatsiya jarayonini samarali tashkil etish muhim vazifalardan biri hisoblanadi.

Defosforatsiya metall va shlak o'rtasida kechadigan murakkab fizik-kimyoviy jarayon bo'lib, unda metall tarkibidagi fosfor oksidlanuvchi sharoitda yani temir oksidi (FeO) ishtirokida reaksiyaga kirishib, shlak tarkibiga o'tadi. Jarayon samaradorligi haroratga, shlak tarkibi va asosililigi,

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kislorod potentsiali hamda aralashirish darajasiga bog'liq. Yuqori asosli (kalsiy oksidiga boy) shlaklardan foydalanish defosforatsiya jarayonini yaxshilaydi, biroq haroratning ortishi muvozanatga salbiy ta'sir ko'rsatadi.

20ГJI - bu transport mashinasozligida keng foydalaniladigan, kam uglerodli va kam legirlangan, quyma yo'li bilan olingan konstruksiyon po'latdir. Ushbu markali po'lat uchun defosforatsiya jarayoni o'rganish alohida ahamiyatga ega, chunki uning mexanik hamda ekspluatatsion xossalari yuqori darajada bo'lishi talab etiladi. Fosfor miqdorini kamaytirish metall sifatini oshirish va uning xizmat muddatini uzaytirishda muhim rol o'ynaydi. Shu sababdan ishning maqsadi - 20ГJI markali po'lat eritishda defosforatsiya jarayonini va mexanizmini o'rganish hamda unga ta'sir etuvchi asosiy omillarni aniqlashdan iborat.

## 2. Tadqiqot metodologiyasi

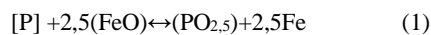
Defosforatsiya jarayonini termodinamik tahlil qilish uchun 20ГJI markali po'lat tanlab olingan. 1-jadvalda ushbu po'latni va shlakning kimyoviy tarkibi 720 ta erish jarayonidagi tarkibning o'rtachasi olinib, termodinamik hisob-kitoblarni tahlil qilgan.

1-jadval

Defosforatsiya jarayonidagi metall va shlakning o'rtacha kimyoviy tarkibi

20ГJI markali po'latning kimyoviy tarkibi, % (mass.)						
C	Si	Mn	P	S	Al	Fe
0,16	0,08	0,12	0,045	0,04	0	qolgan
Defosforatsiya jarayonida 20ГJI markali po'latning eritishdagi shlak tarkibi, % (mass.)						
CaO	SiO <sub>2</sub>	MnO	Al <sub>2</sub> O <sub>3</sub>	MgO	FeO	Umumiy
50	16	6	3	10	15	100
Shlakdagi kationlarning molyar ulushlari						
56	60	71	102	40	72	n <sub>i</sub>
Shlakdagi har bir komponentning molyar miqdori						
0,893	0,267	0,085	0,029	0,250	0,208	$\sum n_i = 1,761$
Metall ionlarining umumiy ionlar yig'indisidagi ulushi						
0,507	0,151	0,048	0,033	0,142	0,118	1

Defosforatsiya jarayoni (1) reaksiya orqali yozilib, bu reaksiyani Gibbs energiyasi (2) ifodaga tengdir:



$$\Delta G_{um} = 20537 + 24,65T \quad (2)$$

Pechdagi suyuq metall haroratini 1800 K dan 1925 K gacha 25K qadam bilan o'zgartirildi. Muvozanat konstantasi Vant-Goff tenglamasidan foydalanib keltirib chiqarildi. Vant-Goff tenglamasi yoki izoterma reaksiya tenglamasi deb nomlanuvchi bu formula kimyoviy reaksiyaning standart Gibbs energiyasi ( $\Delta G_{um}$ ) va muvozanat konstantasi ( $K$ ) o'rtasidagi bog'liqlikni ifodalaydi va (3) ifodadan topiladi:

$$\lg K_p = -\frac{\Delta G_{um}}{2,3RT} = -\frac{(20537+24,65T)}{2,3 \cdot 8,314 \cdot T} \quad (3)$$

bu yerda:  $R = 8,314 \text{ J}/(\text{mol} \cdot \text{K})$  - universal gaz doimiysi;

$$T = (1800 \dots 1923) \text{K} - \text{harorat.}$$

Ikkinchi tarafdan, 4-tenglamaga ko'ra muvozanat doimiysi (3) ifodaga teng va quyidagicha topiladi.

$$K_p = \frac{a_{PO_{2,5}} \cdot a_{Fe}^{2,5}}{a_P \cdot a_{FeO}} = \frac{x_{P^{5+}}}{[P]} \cdot \frac{\gamma_{P^{5+}}}{f_P \cdot a_{FeO}^{2,5}} \Rightarrow \left[ \begin{aligned} a_{Fe} = X_{Fe} = 1 & \quad a_{PO_{2,5}} = X_{P^{5+}} \cdot \gamma_{P^{5+}} \\ a_P = [P] \cdot f_P & \quad X_{P^{5+}} = 2 \cdot \frac{(P_2O_5)}{\mu_{P_2O_5}} = \frac{(P)}{\mu_P \cdot \sum n_i} \end{aligned} \right] \Rightarrow \frac{(P)}{[P]} \cdot \frac{\gamma_{P^{5+}}}{31 \cdot \sum n_i \cdot f_P \cdot a_{FeO}^{2,5}}; \quad (4)$$

bu yerda:  $a_{PO_{2,5}}$ ,  $a_{FeO}$ ,  $a_P$ ,  $a_{Fe}$ , - fosfor va temir oksidi, fosfor hamda temir aktivligi;

$[P]$ , - metal tarkibidagi fosfor va kislorodning miqdori, %;

$f_P$  - fosforning aktivlik koeffitsiyentlari. 2-tenglamadan foydalanib turli harorat uchun muvozanat konstantasi hisoblanadi. Fosforning aktivlik koeffitsiyentini turli harotlarda hisoblash uchun 5- ifodadan foydalanildi.

$$\lg f_P = \frac{T}{1873} \cdot (e_P^C [C] + e_P^{Mn} [Mn] + e_P^{Si} [Si] + e_P^R [R] + e_P^S [S] + e_P^{Al} [Al]); \quad (5)$$

bu yerda:  $e_P^R [R]$  - metal tarkibidagi  $[R]$  komponentining fosfor bilan ta'sirlashish parametri.

Metall tarkibidagi komponentlarning fosfor bilan ta'sirlashish parametrlari 2-jadvalda keltirilgan.

2-jadval

Birinchi tartibli ta'sirlashish parametrlari

$e_P^R$	[C]	[Si]	[Mn]	[P]	[S]	[Al]
$e_P$	0,13	0,12	0	0,062	0,028	0

Fosforning taqsimlanish koeffitsienti formulasi quyida keltirilgan:

$$L_P = \frac{(P)}{[P]}; \quad L_P = \frac{31 \cdot K \cdot \sum n_i \cdot f_P \cdot a_{FeO}^{2,5}}{\gamma_{P^{5+}}} \quad (6)$$

Metall va shlak orasidagi fosforning taqsimlanish koeffitsiyentini ( $L_P$ ) bilgan holda metalldagi  $[P]_{ox}$  va shlakdagi  $(P)_{ox}$  fosforning oxirgi konsentratsiyalarini topish mumkin. Buning uchun (7) hamda (8) formulalardan foydalanib tenglamalar sistemasi tuziladi:

$$L_P = \frac{(P)_{ox}}{[P]_{ox}} \quad (7)$$

$$m_m [P]_b + m_s (P)_b = m_m [P]_{ox} + m_s (P)_{ox}; \quad (8)$$

bu yerda:  $m_m$  va  $m_s$  - metall va shlak massasi;  $[P]_b$  va  $(P)_b$  - metall va shlakdagi fosfor boshlang'ich konsentratsiyalari;

$[P]_{ox}$  va  $(P)_{ox}$  - metall va shlakdagi fosforning oxirgi konsentratsiyalari.

Ma'lumki, (8) ifoda materiallar balansi tenglamasi bo'lib, fosfor gaz fazasiga ajralmasdan, faqat metall va shlak orasida qayta taqsimlanishi sharti bilan tuzilgan. Agar eritish jarayonida  $m_m$  va  $m_s$  kattaliklar o'zgarmasa, u holda (7) va (8) tenglamalar sistemasini yechib, metalldagi fosforning oxirgi miqdorini hisoblash ifodasini (9) tenglama bo'yicha topiladi:

$$[P]_{ox} = \frac{100[P]_{bosh} + \lambda(P)_{bosh}}{100 + \lambda L_P} \quad (9)$$

bu yerda  $\lambda = m_{sh}/m_{met}$  - shlak karraligi, %.

Defosforatsiya darajasini (10) formula yordamida topiladi:

$$\eta_{LP} = \frac{[P]_b - [P]_{ox}}{[P]_b} \cdot 100\%;$$

yoki



$$\eta_P = \frac{\lambda(L_K - (P)_b / [P]_b)}{1 + 0,01\lambda L_K} \quad (10)$$

Agar shlakning tarkibi defosforatsiya shartlarini va metall va shlak takibidagi elementlarning o'rtasida taqsimlanishining moddiy muvozanatini qoniqtirmasa, masala iteratsion yaqinlashish usuli bilan yechiladi. Agar element taqsimotining materiallar balansi mos kelmasa - jarayon sharoitida qabul qilingan kuyish koeffitsiyentini o'zgartirish kerak. Agar shlak tarkibi defosforatsiya sharoitini qoniqtirmasa temir oksidi (FeO) miqdorini oshirish talab etiladi. Shlak tarkibi tuzatilgandan so'ng, jarayonni takrorlash zarur.

Ushbu usul bo'yicha, masalan, fosforni, oltingugurti va boshqa elementlarning ham pechda va pechdan tashqarida rafinirlash uchun shlak miqdorini, qattiq shlak aralashmasining sarfini, tizimning zarur oksidlanishini, jarayon haroratini hamda defosforatsiya jarayonining boshqa texnologik parametrlarini hisoblash mumkin.

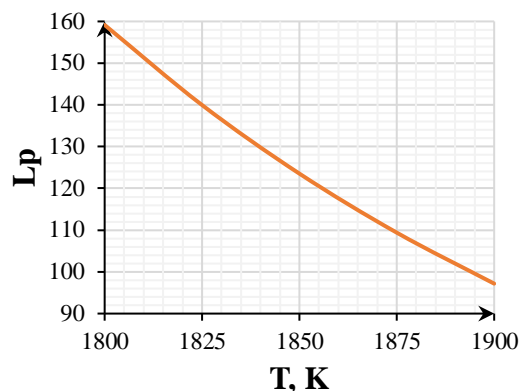
3-jadval

### Defosforatsiyadagi barcha jarayonlarning haroratga bog'liqligi

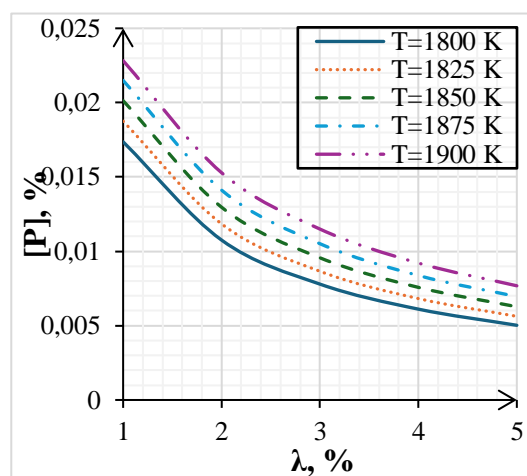
Ko'rsatkichlar	Absolyut harorat (T), K				
	1800	1825	1850	1875	1900
$G^T$ , J/mol	23836	24452	25069	25685	26301
lgKp	-0,693	-0,701	-0,709	-0,716	-0,724
Kp	0,203	0,199	0,196	0,192	0,189
$\sum ni$	1,761	1,761	1,761	1,761	1,761
$\ln \gamma_{Fe^{2+}}$	0,762	0,752	0,742	0,732	0,722
$\gamma_{Fe^{2+}}$	2,143	2,121	2,100	2,079	2,059
$\ln \gamma_{P^{5+}}$	-6,013	-5,931	-5,850	-5,772	-5,696
$\gamma_{P^{5+}}$	0,002 4	0,002 7	0,002 9	0,003 1	0,003 4
lgfp	0,036	0,035	0,035	0,034	0,034
fp	1,086	1,084	1,083	1,082	1,081
$a_{FeO}$	0,254	0,251	0,248	0,246	0,244
$L_P$	159	140	124	109	97
Metalldagi fosforni oxirgi miqdori [P] ( $\lambda$ ), %					
$\lambda=1$ %	0,017	0,019	0,020	0,021	0,023
$\lambda=2$ %	0,011	0,012	0,013	0,014	0,015
$\lambda=3$ %	0,008	0,009	0,010	0,011	0,011
$\lambda=4$ %	0,006	0,007	0,008	0,008	0,009
$\lambda=5$ %	0,005	0,006	0,006	0,007	0,008
Defosforatsiya darajasi, $\eta$ ( $\lambda$ ), %					
$\lambda=1$ %	61	58	55	52	49
$\lambda=2$ %	76	74	71	69	66
$\lambda=3$ %	83	81	79	77	74
$\lambda=4$ %	86	85	83	81	80
$\lambda=5$ %	89	87	86	85	83

Quyidagi jadvaldagi ko'rsatkichlardan foydalanib, defosforatsiyadagi ba'zi asosiy jarayonlarning harorat

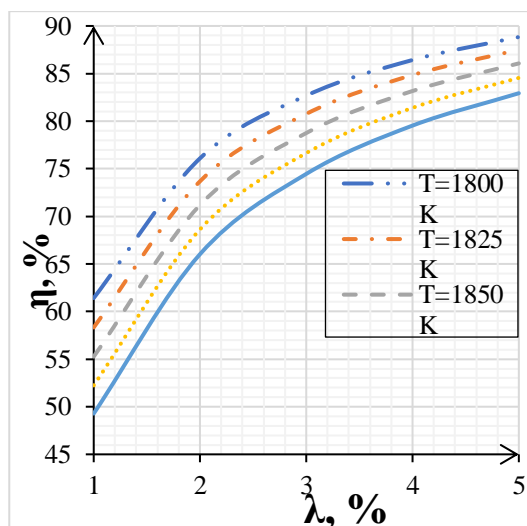
ta'sirida qanday o'zgarishini 1-2-3-grafiklardan aniqroq tushunib olishimiz mumkin.



1-rasm. Fosforning taqsimlanish koeffitsiyentining haroratga bog'liqlik grafiqi



2-rasm. Turli haroratlarda metalldagi fosforning oxirgi konsentratsiyasining shlak karraliligiga bog'liqlik grafiqi



3-rasm. Turli haroratlarda shlak karraliligiga bog'liq holda defosforatsiya darajasi o'zgarishi grafiqi



Hisobiy jadval va grafiklardan ko'rinib turibdiki, harorat 1800K dan 1900K gacha ortishi bilan fosforning taqsimlanish koeffitsiyenti kamayadi. Ushbu haroratlarda shlak karraliligi foizi ortishi bilan metallidagi fosforning oxirgi konsentratsiyasini miqdori kamayadi, bu esa defosforatsiya darajasini oshishiga olib keladi.

### 3. Xulosa

Termodinamik tahlillar yordamida, 20GL markali quyma po'latni tarkibidagi legirovchi elementlarning (C, Si, Mn, Cr, Ni, Cu, Al) fosfor aktivligiga ta'siri o'rganildi. Aniqlanishicha, po'lat tarkibidagi uglerod (0,20%) va kremniy (0,35%) elementlari fosforning aktivlik koeffitsiyentini oshirib, uning metall fazasidan shlak fazasiga o'tishi uchun qulay termodinamik sharoit yaratadi. Tadqiqotlar natijasida fosforning muvozanat konsentratsiyasi harorat ko'tarilishi bilan chiziqli ravishda kamayishi kuzatildi. Harorat 1525°C dan 1625°C gacha o'sishi bilan fosforning shlakka o'tish samaradorligi pasayadi. Bu esa defosforatsiya jarayonining ekzotermik tabiatini tasdiqlaydi va jarayonning yakuniy bosqichida metall haroratini 1540...1550°C atrofida ratsionallashtirish zarurligini ko'rsatadi. Bundan tashqari, fosforning metall va shlak fazalari o'rtasidagi taqsimlanish koeffitsiyenti  $L_p$  shlakning asosiyli va oksidlanish salohiyatiga bevosita bog'liqligi o'rganildi. Shlakning asosiyli (B) 2,8...3,2 oralig'ida bo'lganda,  $L_p$  ko'rsatkichining eng yuqori qiymatlariga erishilishi, bu esa metall tarkibida fosfor miqdorini minimal darajaga tushirish imkonini berishi isbotlandi. Aniqlangan qonuniyatlar 20GL markali po'latdan tayyorlanadigan transport detallarining sovuqqa chidamlilik, zarbiy qovushqoqlik xususiyatlarini oshirishga va ularning past haroratlarda ishonchligi va umrboqiyilgini ta'minlashga xizmat qiladi.

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<b>Z. Adilova, S. Setimbetova</b>	
<i>International transport corridors and Uzbekistan's integration into the global logistics system method.....</i>	<i>50</i>
<b>N. Tursunov, A. Saidirakhimov, N. Kodirova, Z. Rakhmatova</b>	
<i>Investigation of the mechanism and factors influencing the process of dephosphorization during the smelting of 20GL steel.....</i>	<i>54</i>
<b>G. Khalmatjanova</b>	
<i>Methods of designing cotton and textile clusters in the agro-industrial complex.....</i>	<i>58</i>
<b>A. Rakhmanov, E. Abdusamatov, Sh. Shermatov, U. Isokhanov</b>	
<i>Analysis of methods for formalizing road traffic accidents.....</i>	<i>63</i>
<b>A. Lesov, S. Yuldasheva</b>	
<i>Analysis of the application of renewable energy sources in metro systems.....</i>	<i>68</i>
<b>Z. Adilova, M. Sharapova</b>	
<i>Analytical foundations of container transportation management.....</i>	<i>73</i>
<b>Kh. Nekboev, M. Suvonkulova</b>	
<i>Application of information systems in the management of transport logistics processes.....</i>	<i>79</i>
<b>N. Sarvirova, D. Tajibaev, D. Khakimov</b>	
<i>Formalized selection of sites for the ancient Khorezm branded tourist route in Karakalpakstan.....</i>	<i>83</i>
<b>Sh. Khakimov, D. Odilov, U. Isokhanov</b>	
<i>The role of digitalization in increasing the efficiency of truck utilization .....</i>	<i>88</i>
<b>N. Arifjanova</b>	
<i>Implementation of internet of things (IoT) technologies for warehouse logistics optimization: Domestic and foreign experience.....</i>	<i>92</i>
<b>D. Ayrapetov, R. Khakimov</b>	
<i>Restoration of the thermophysical properties of antifreezes via a regeneration method based on regression analysis.....</i>	<i>95</i>